



Distortion Identification and Quantification: Advances Supporting Facilities Design

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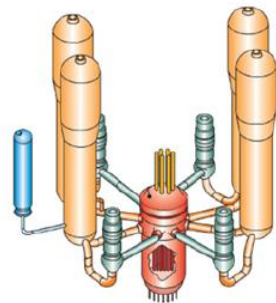
Agenda

- **Some works on distortions quantification:**
 - **Hybrid approach: “a generalized distortion correction strategy”**
 - **Sensitivity analysis in support of distortions quantification**
- **Development of a scaling tool in CATHARE code**



Context

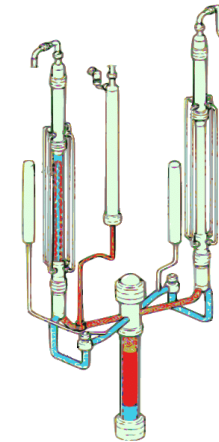
« **Scaling** » in support of the facility design: Does the scaling analysis ensure that the studied installation/scenario/transient is representative of the full-scale reactor case?



Reactor Scale

Scaling analysis:

1. Thermal hydraulic analysis
2. Order of magnitude
3. PIRT
4. Design criteria



Reduced scale

Scaling analysis:

1. Thermal hydraulic analysis
2. Order of magnitude
3. PIRT
4. Design criteria
5. Distortion analysis (H2TS, FSA, DSS..)



Scaling analysis

Identification of transient
(safety issues)

Identification of thermal
hydraulic phenomena
(THPs), FoM and Pol

Identification of
bifurcating events (BEs)

Identification of scaling
equations

Choice of scaling
methods

Phenomena Identification
and ranking table (PIRT)

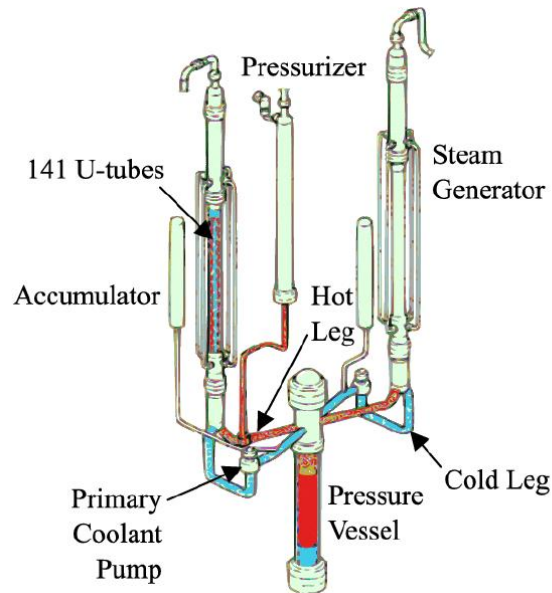
Facilities
Design

Distortions
evaluation

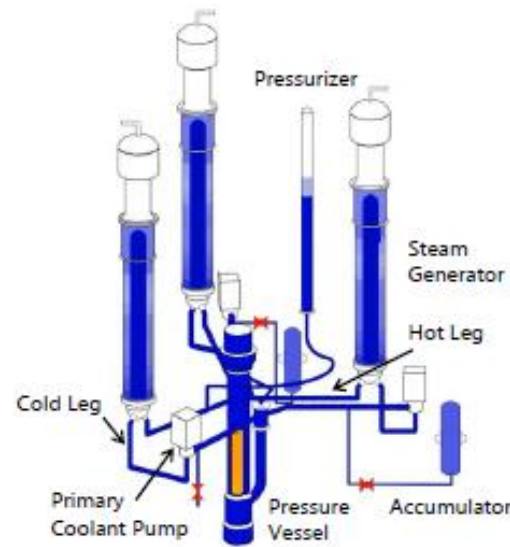
How can we better quantify the distortions, and their impact on the reference transient?

A generalized distortion correction strategy

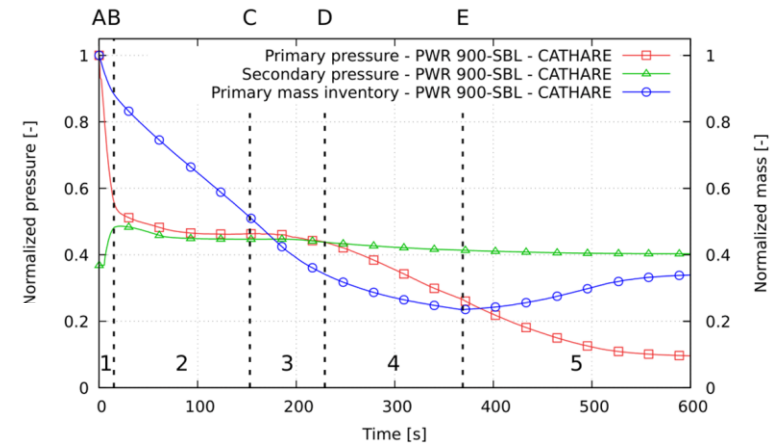
Example of a 6% CL break: LSTF, BETHSY and reactor scale



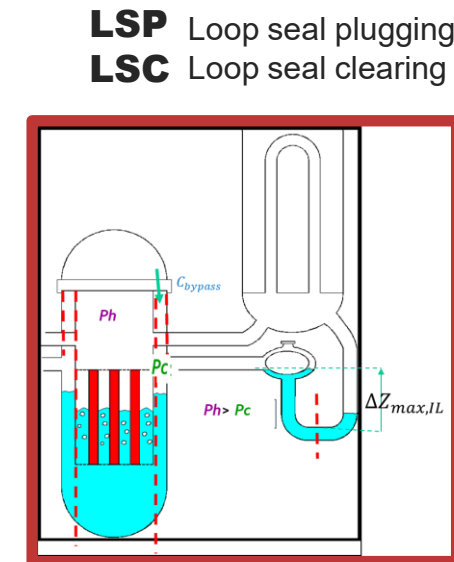
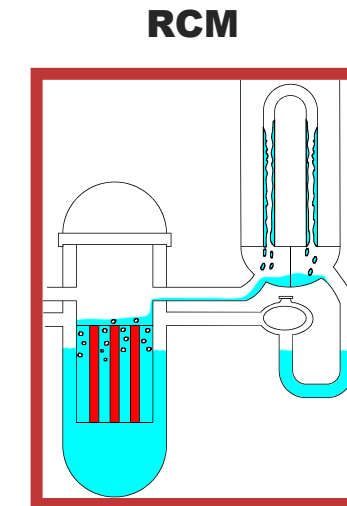
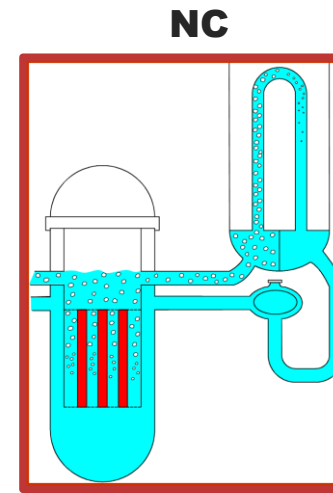
LSTF: Vol: 1/48, H: 1/1, PWR-4L



BETHSY: Vol: 1/100, H: 1/1, PWR-3L



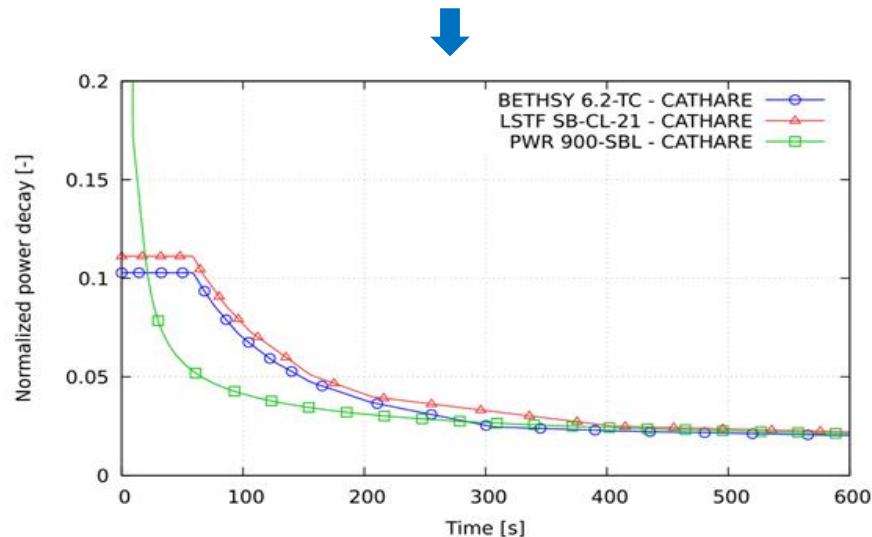
- 1: Subcooled Blowdown
- 2: Natural Circulation (NC)
- 3: Reflux Condenser Mode (RCM)
- 4: High Quality Break Discharge
- 5: Refill by accumulators



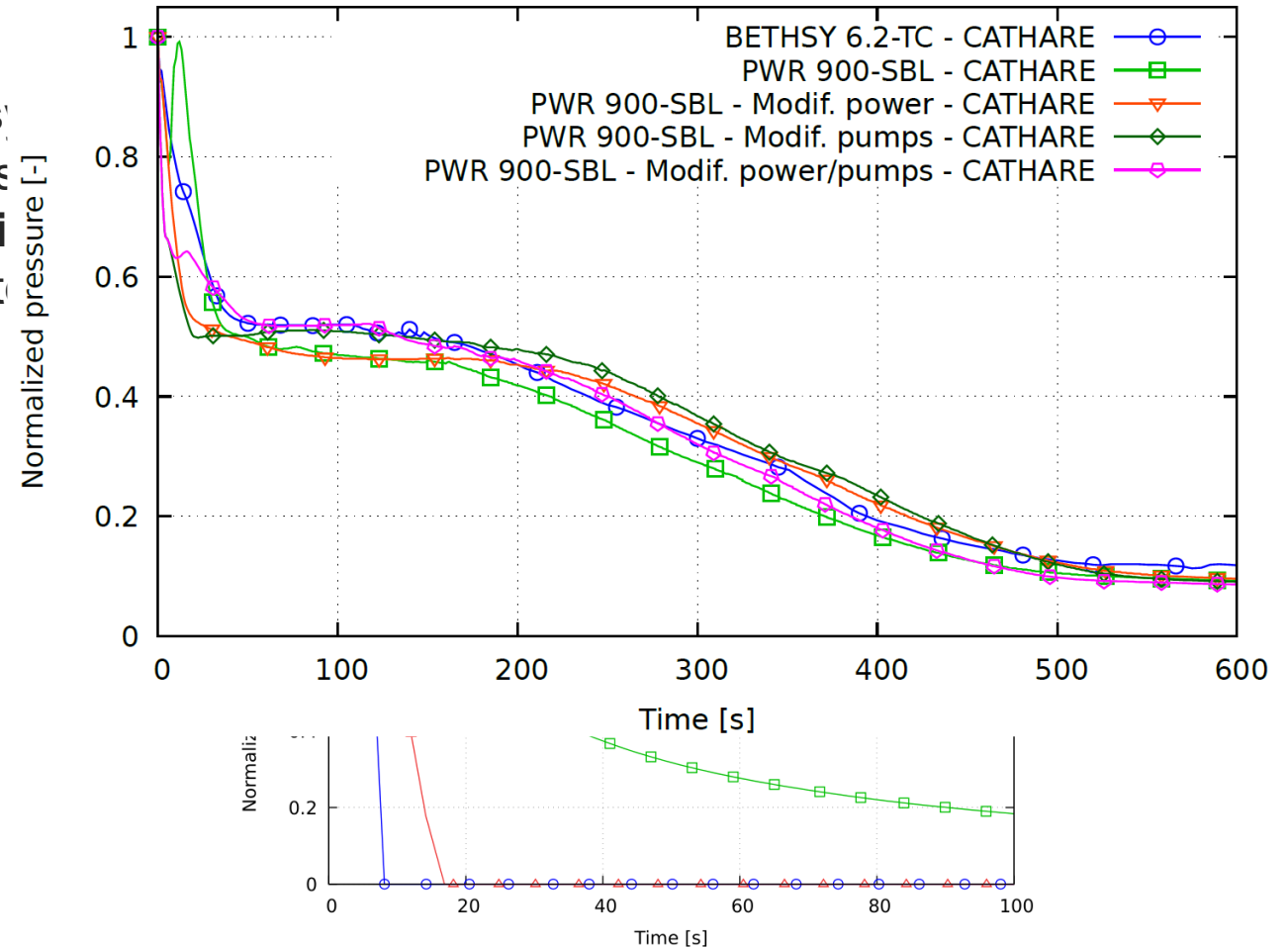
A generalized distortion correction strategy

Some important conclusions:

1. Scaling analysis of three different scaled s
2. Identification of **distortions** and their origins
3. First application of “**a generalized distorti**” by CEA in order to identify and correct dist



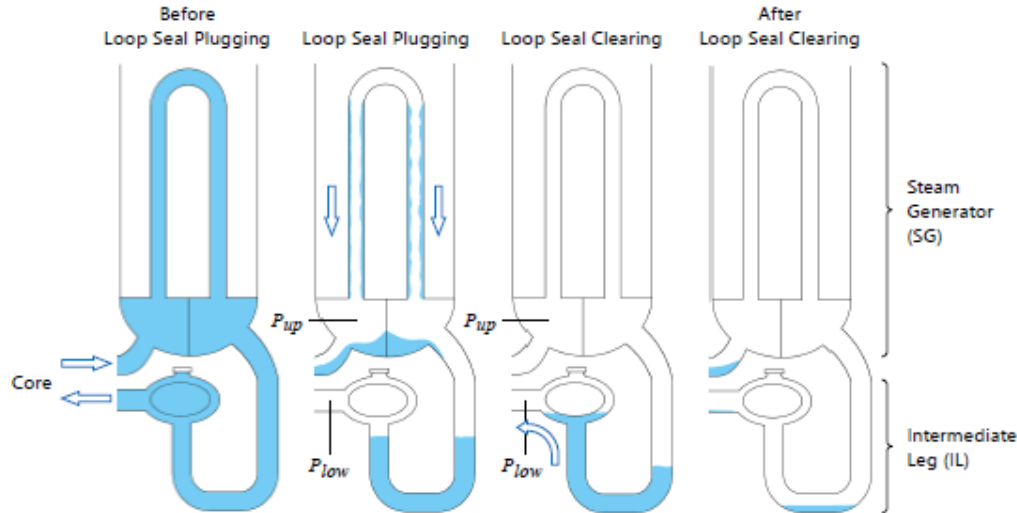
*Distortion of BIC: decay power heat →
correction of distortion by CATHARE →
quantification of distortion and their origins*



*Distortion of design: pump modelling → correction of distortion by
CATHARE → quantification of distortion and their origins*

A generalized distortion correction strategy

Some exceptions : analysis of the LSP and LSC in a SBLOCA simulated by CATHARE

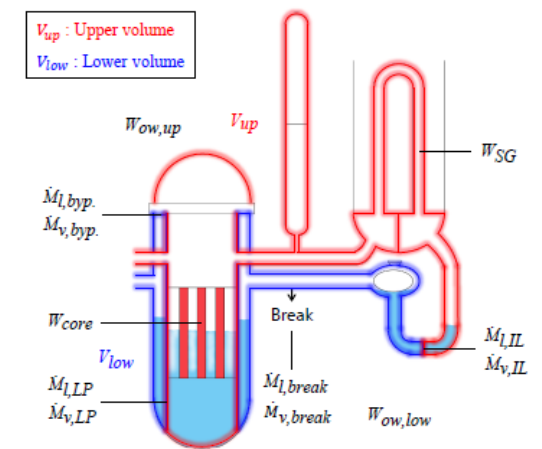


Prediction of the LSC/LSP is challenging for system codes

→ The analysis of BESTHY facility is performed starting from a **pressure balance equation** of the upper and bottom part of the loop. A scaling analysis is performed starting from the **experimental results**

Some important conclusions:

1. Contribution of the scaling analysis without the support of system codes.
2. Top-down approach
3. Characterization of the LPP/LSC and its impact on the PCT
4. Identification of important processes → sensitivity analyses



The sensitivity analysis (GSA) in support of the scaling

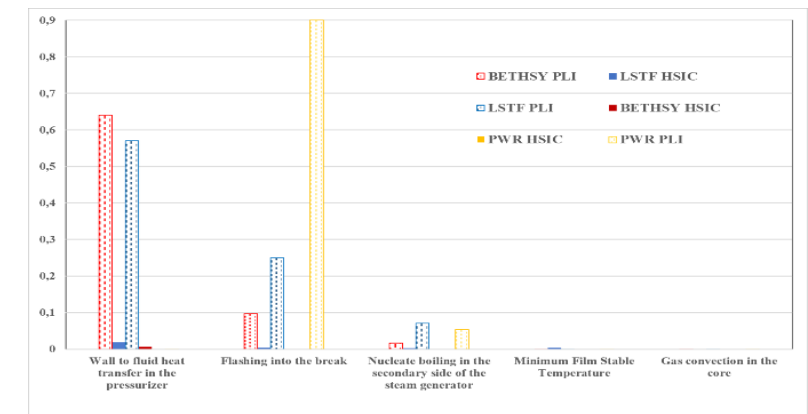
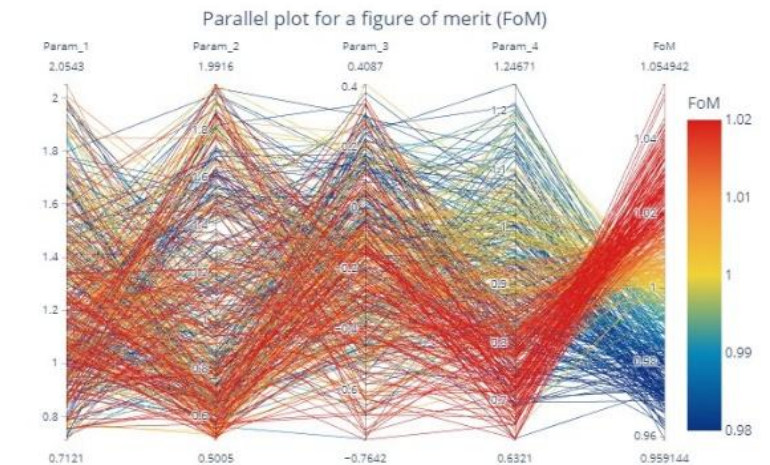
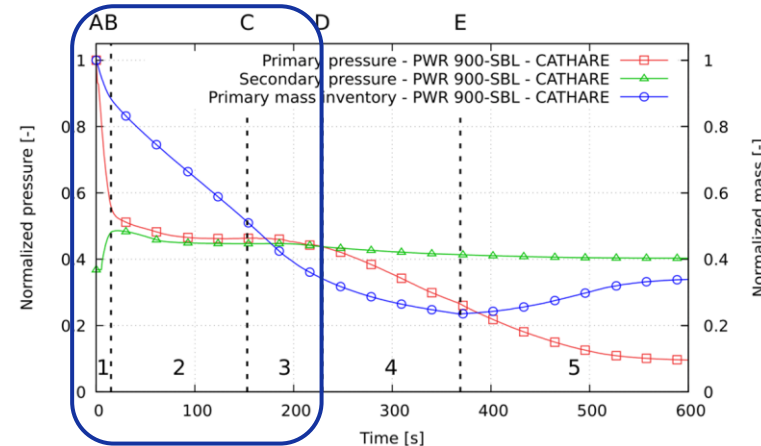
Objectif : the complementarity of the Scaling Analysis and the Generalized Sensitivity Analysis (GSA)

Application of the GSA to the SB-LOCA counterpart test performed in BETHSY, LSTF and reactor case. Focus on:

- Blowdown
- Natural circulation phase
- Reflux mode

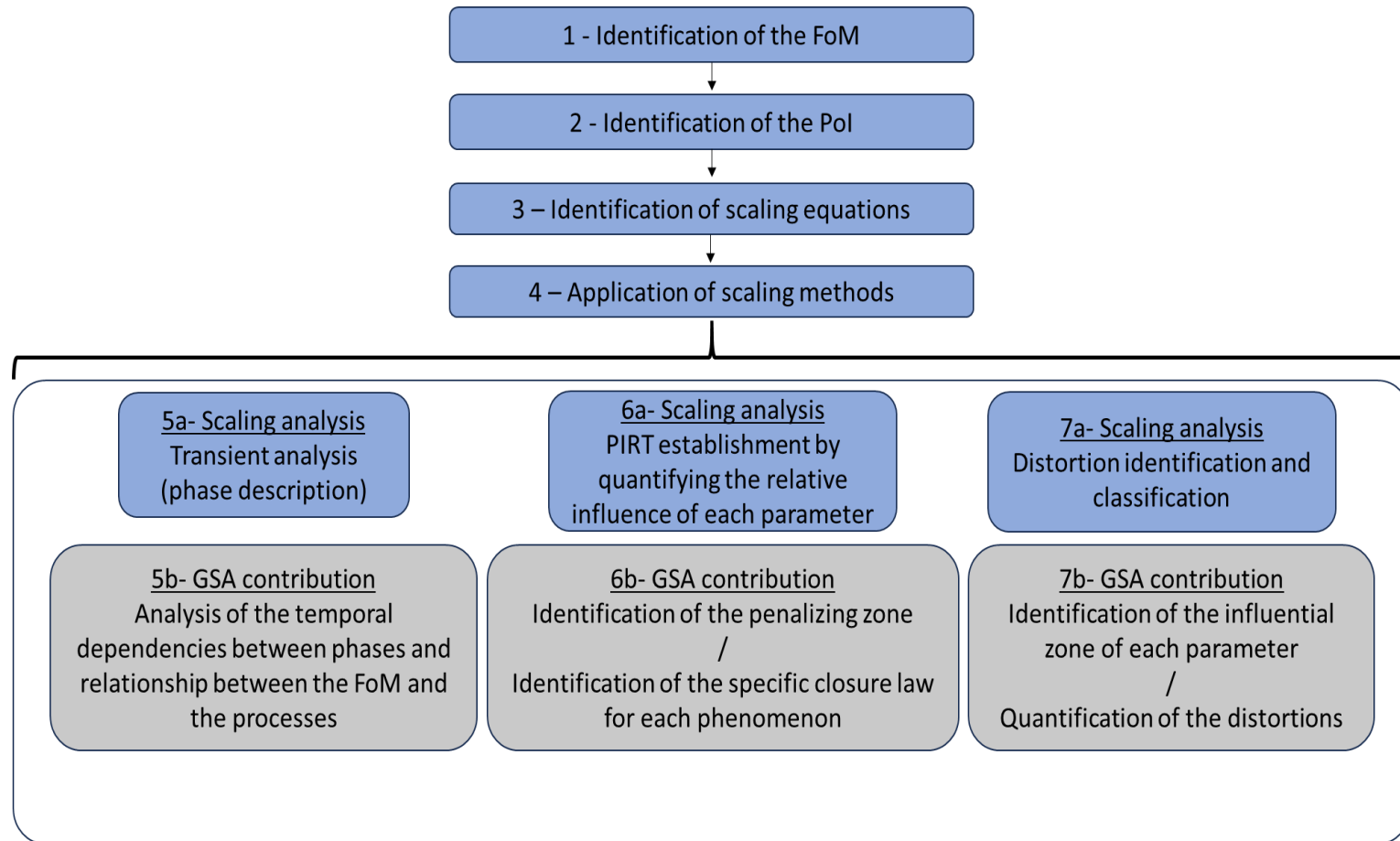
A possible synergy observed in:

- ☐ Transient analysis
- ☐ PIRT establishment
- ☐ Distortions quantification



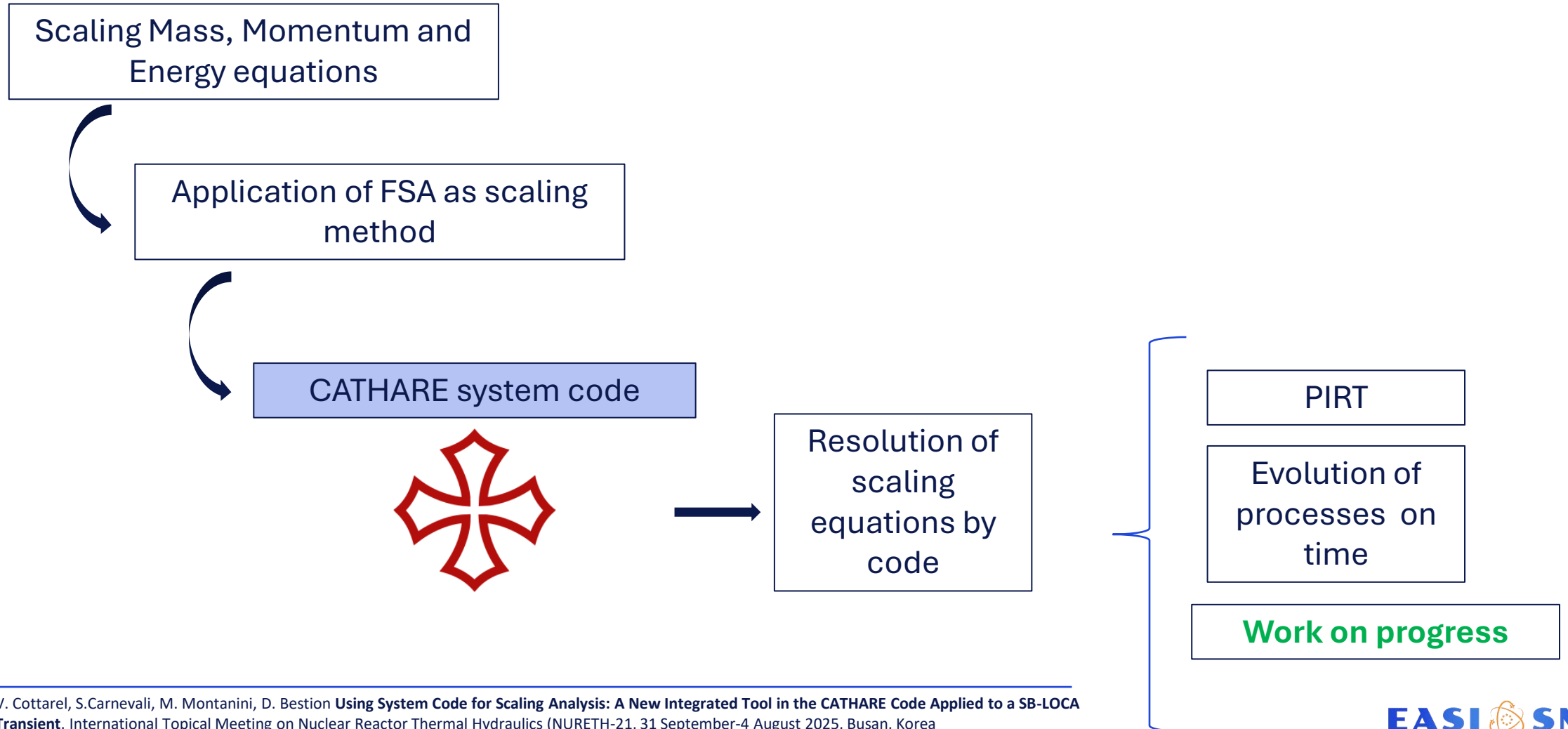
The sensitivity analysis (GSA) in support of the scaling

Some first conclusions GSA + scaling:



Development of a scaling tool in CATHARE code

System code instrumentation with a « scaling » option



Development of a scaling tool in CATHARE code

Resolution of balance equations for a control volume

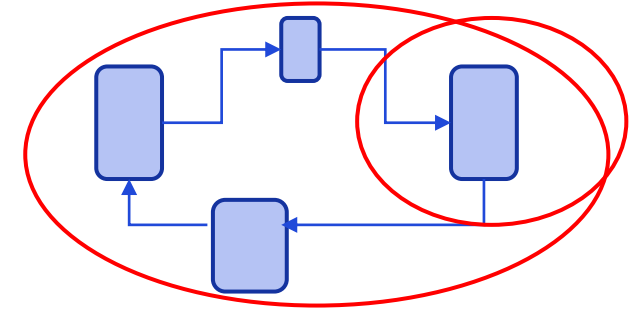
Mass balance

$$\frac{dM_1}{dt} = \dot{M}_{IS} - \dot{M}_{l,br} - \dot{M}_{v,br}$$

Pressure equation (from mass & energy equations)

$$\begin{aligned} &(\mu_l M_l + \mu_v M_v) \dot{P} = \\ &\dot{M}_{l,in} [\nu_l + \nu'_{l,h} (h_{l,in} - h_l)] \\ &+ \dot{M}_{v,in} [\nu_v + \nu'_{v,h} (h_{v,in} - h_v)] \\ &- \dot{M}_{l,out} \nu_l - \dot{M}_{v,out} \nu_v \\ &+ \nu'_{l,h} W_{wl} + \nu'_{v,h} W_{w,v} \\ &+ \nu'_{v,h} W_{iv} + \nu'_{l,h} W_{il} \\ &-(W_{iv} + W_{il}) / \varpi \\ &+ W_{w,i} / \varpi \end{aligned}$$

- liquid & vapor isentropic expansion by P change
- Volume flowrate + thermal expansion of entering liquid
- Volume flowrate + thermal expansion of entering vapor
- Volume flowrate of exiting liquid and vapor
- thermal expansion of liquid & vapor by wall HX
- thermal expansion of liquid & vapor by interfacial HX
- vaporization / condensation due to interfacial HX
- vaporization / condensation due to the walls

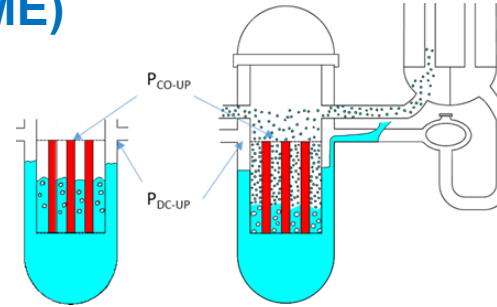


System Pressure evolution governs the timing of many Bifurcating Events (BEs)

Development of a scaling tool in CATHARE code

Integrated Mixture Momentum Equation (MME)

...in a open loop:



$$\Delta P_{AB} \cong \Delta P_{gr} + \Delta P_{sing} + \Delta P_w + \Delta P_{pump} + \Delta P_{IS} + \Delta P_{br}$$

MME controls the relation $\dot{M} \rightarrow (\Delta P_{pump}, \Delta P_{grav}, \Delta P_{fr}, \Delta P_{sing})$

Integrated Crossed Momentum Equation (CME)

$$\alpha_l MomEq_v + \alpha_v MomEq_l$$

$$\Delta P_{AB} \cong \Delta P_{buo} + \Delta P_{sing} + \Delta P_w + \Delta P_{pump} + \Delta P_{acc} + \Delta P_{IS} + \Delta P_{br} + \Delta P_{addM} + \Delta P_{inter}$$

CME controls the local slip ratio

Development of a scaling tool in CATHARE code

Rate of mass change due to the contribution of :

SBD phase

Liquid entering
Gas entering
Liquid exiting
Gas exiting

**Results from
Ciechocki [3]**

-
-
-1.000*
-0.013*

**Results from
supervisor**

0.355
0.020
-1.000
-0.013

NC phase

Liquid entering
Gas entering
Liquid exiting
Gas exiting

-
-
-1.000*
-0.087*

0.001
0.012
-1.000
-0.085

RR phase

Liquid entering
Gas entering
Liquid exiting
Gas exiting

1.000†
-
-0.022*
-0.464*

1.000
0.022
-0.041
-0.972

**Effect metrics of
the primary system
during the
transient**

Additional
investigation

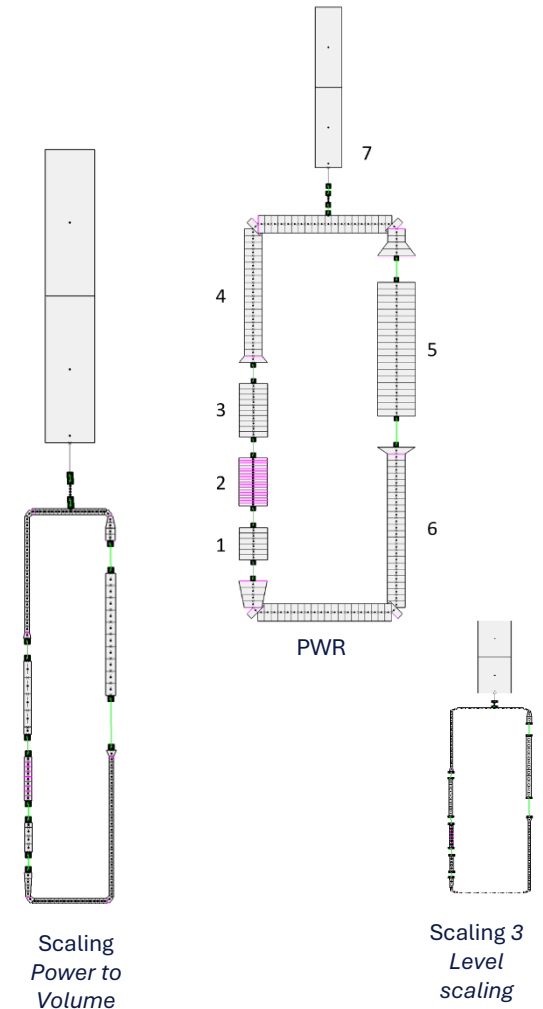
Distortions in passive systems

« Scaling analysis » in support of the passive systems (PhD of M. MONTANINI, Université Paris-Saclay)

□ Development and application of the momentum equations:

- Mixing : gas + liquid → global fluid behavior
- Crossed : $\alpha_l MomEq_v + \alpha_v MomEq_l$ → interfacial friction

□ Impact of the design to the system behavior



Perspectives

- Application of *a generalized distortion correction strategy* to additional transients
- Investigation of the **GSA** in support of the scaling analysis: additional application cases
- Finalization of **CATHARE** scaling tool
- Scaling analysis of **passive systems** in support of distortions assessment

Thank you

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